

Improvement of Transient Response of a DC Motor Controller Based on Non-Linear Optimization Techniques

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Abstract— In this study, various precise and appropriate control systems that use a DC motor, have been simulated for improved transient response. Three controllers: lead-lag compensator, conventional Proportional-Integral-Derivative (PID) and Fuzzy logic controller were designed and simulated in order to analyse the performance. Among them, Fuzzy logic algorithm tuning for PID controller exhibits better transient response for DC motor actuators.

Index Terms— DC motor, Fuzzy logic, Lead compensator, Lead Lag compensator, Proportional-Integral-Derivative controller, Transient response

I. INTRODUCTION

Owing to their high reliabilities, flexibilities, and low costs, DC motors are widely used in industrial applications, robot manipulators and home appliances. There are several types of applications where the load on the DC motor varies over a speed range. These applications demand speed control accuracy and good dynamic responses [1,13]. So, it is important to introduce a controller to control the speed and transient behavior of a DC motor in the desired manner.

Today, more than 95% of control design applications utilize Proportional-Integral-Derivative(PID) [2,14]. The PID controllers are commonly used for motor control applications because of their simple structures and comprehensible control algorithms [3,4]. Two main problems encountered in motor control are the time-varying nature of motor parameters under operating conditions and the existence of noise in a system loop. Analysis and control of complex, nonlinear and time-varying systems is a challenging task using conventional methods because of uncertainties. The fuzzy set theory which led to a new control method called Fuzzy Control is able to cope with system uncertainties [5,6]. One of the most important advantages of fuzzy control is that it can be successfully applied to control nonlinear complex systems. Moreover, PID controller requires a mathematical model of the system while Fuzzy logic controller (FLC) provides an alternative to PID controller, especially when data are not available or partly available for the system [6,7].

In this paper, a conventional PID controller, a lead-lag compensator filter and a Fuzzy logic controller for DC motor actuators have been designed. The simulation was performed to show the response for each proposed design. The research tool for this work was MATLAB and Simulink where simulations were done and appropriate behaviors regarding each controller were observed.

A linear differential equation describing the properties of a

DC motor to model the relation between input (V) and output ($\dot{\theta}$) was first developed. From that, a transfer function was derived. This transfer function was then used to analyze the performance of the system and to design proper controllers to meet the design criteria. For the compensator design, the locations of the desired poles were found out from the proposed values of settling time, rise time and percentage overshoot [8,9]. Using root locus, it was found that a lead compensator is required to place poles in the desired locations. A lag compensator was also designed and added to meet the steady-state requirement of the problem. Further, a PID controller was designed and tuned based on the conventional methods [10,14]. To achieve smoother control, a fuzzy logic controller with two inputs and one output including several rules was also designed [11]. All the four controllers were implemented in the simulation. In fine, the controllers were compared against each other based on their performance and control.

II. DYNAMICS OF A DC MOTOR

The most common device used as an actuator in mechanical control is the DC motor. The physical parameters of the motors are:

TABLE I
MOTOR DYNAMICS

Parameters	Selected Values
Moment of inertia of the rotor, J	$42.6 \times 10^{-6} \text{ Kgm}^2$
Viscous friction coefficient, b	$47.8 \times 10^{-6} \text{ Nms}$
Torque constant, k_t	$14.5 \times 10^{-3} \text{ Nm/A}$
Back emf, k_e	$14.5 \times 10^{-3} \text{ Vs/rad}$
Terminal resistance, R	4.57Ω
Electric inductance, L	$171 \times 10^{-3} \text{ H}$

The motor speed for a given voltage is given by the law of physics described by the open-loop transfer function (1) in Laplace domain with voltage V(s) as input and shaft speed $\omega = \dot{\theta}(s)$ as output. The relationship between the reference speed $\dot{\theta}_{ref}$ and the output speed $\dot{\theta}(t)$ with a constant gain of K is given by the closed loop transfer function (2). The Routh-Hurwitz MATLAB program was used to check the stability of the system. The state space representation of the plant dynamic as given in (3) was used to confirm that the system is stable, controllable and observable.

$$\frac{\dot{\theta}(s)}{V(s)} = \frac{\frac{K_t}{JL}}{s^2 + \frac{(JR+bL)}{JL}s + \frac{bR+k_e k_t}{JL}} \tag{1}$$

$$\frac{\dot{\theta}_{out}}{\dot{\theta}_{ref}} = \frac{\frac{K.K_t}{JL}}{s^2 + \frac{(JR+bL)}{JL}s + \frac{K.K_t+bR+k_e k_t}{JL}} \tag{2}$$

$$\begin{bmatrix} \dot{i} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} -R/L & -k_e/L \\ k_t/J & -b/J \end{bmatrix} \begin{bmatrix} i \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 1/L \\ 0 \end{bmatrix} V(t)$$

$$\dot{\theta} = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} i \\ \dot{\theta} \end{bmatrix} \tag{3}$$

III. LEAD-LAG COMPENSATOR DESIGN

It is observed from the root locus of the open loop transfer function (Fig. 1) that the system has two real open loop poles at $P_1 = -25.2$ and $P_2 = -2.1$ which repel each other at -14.5 , one going to the positive infinity and other going to the negative infinity. The desired damping ratio ($\xi = 0.69$) and desired natural frequency ($\omega_n = 57.962$ rad/s) were calculated through the available equations for settling time and percentage overshoot and were then used in determining the desired characteristic equation as described in (6). Since the desired poles $S_{1,2} = -40.1 \pm 41.9476i$ do not satisfy the angle condition for the actual characteristic equation as shown in (7), the root locus will not go through the desired poles.

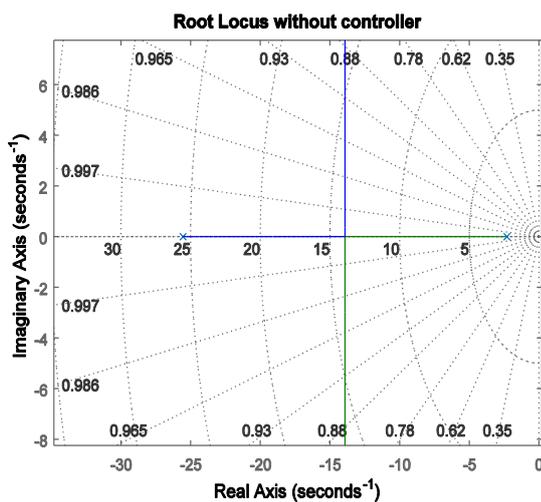


Fig. 1 Root locus of the DC motor system without any controller

Hence a lead compensator filter was required to shift the root locus to the left half plane to meet the desired poles location. The closed loop poles were placed at the desired location by multiplying the lead compensator transfer function

$$G_1(s) = \frac{K_1(s+a_1)}{(s+b_1)}, (|b_1| > |a_1|) \tag{4}$$

to the open loop transfer function of the system and then performing coefficient matching which yields a system of three equations with four unknowns (a_1, b_1, c_1, K_1), where c_1 is the added pole to the desired characteristic equation. The one degree of design flexibility was satisfied by assuming $a_1 = 16$, which results in $K_1=1.2754$, $b_1 = 65.3889$, $c_1= 20.41$. The performance of the designed lead compensator was evaluated for a step input through final value theorem. The limit showed convergence to 0.7% which is larger than the desired SSE of 0.1%, hence a lag compensator with transfer function

$$G_2(s) = \frac{K_2(s+a_2)}{(s+b_2)}, (|b_2| < |a_2|) \tag{5}$$

was added by assuming $a_2 = 5$ resulting $b_2=0.0578$. The final transfer function of the complete lead-lag compensator filter is

$$G_{lead-lag}(s) = G_1(s)G_2(s)$$

$$\Delta_D = s^2 + 2\xi\omega_n s + \omega_n^2$$

$$= s^2 + 79.999s + 3359.59 \tag{6}$$

$$\Delta_D = (s + 40.1 + 41.9476i)(s + 40.1 - 41.9476i) \tag{7}$$

$$G_{lead-lag}(s) = \frac{1.275s^2 + 26.78s + 102}{s^2 + 65.45s + 3.778} \tag{8}$$

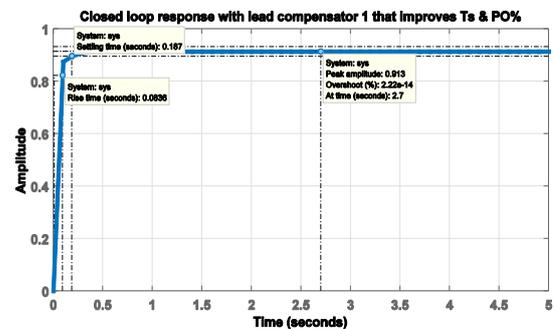


Fig. 2 Closed loop response of lead compensator

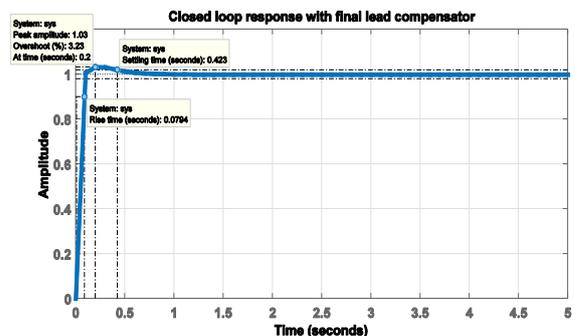


Fig. 3 Closed loop response of final lead-lag compensator

IV. PID CONTROLLER DESIGN

The general transfer function for a PID controller in Laplace domain can be written as shown in (9) where K_p is the proportional gain, K_I is the integral gain and K_D is the derivative gain [12]. Considering the effect of each term in the PID controller the PID gains were selected through a trial and error approach and were then tuned by simulation with final values of: $K_p=0.67$, $K_I=0.55$ and $K_D=0.01$

The open loop and closed loop transfer function of the system with PID controller is given by (10) and (11) respectively:

$$PID(s) = K_p + \frac{K_I}{s} + K_D s \quad (9)$$

$$G_{open_loop_PID}(s) = \frac{19.91s^2 + 1334s + 1095}{s^3 + 27.85s^2 + 58.85s} \quad (10)$$

$$G_{closed_loop_PID}(s) = \frac{19.91s^2 + 1334s + 1095}{s^3 + 47.75s^2 + 1392s + 1095} \quad (11)$$

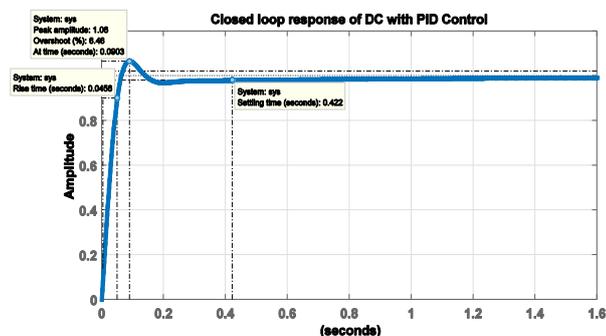


Fig. 4 Closed loop response of PID controller

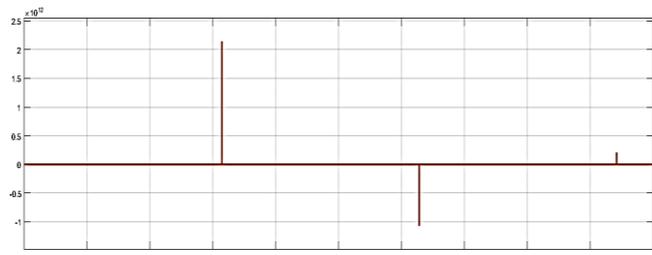


Fig. 5 Plot of control signal for the PID controller for step input

V. FUZZY LOGIC CONTROLLER DESIGN

Fuzzy Inference System (FIS) is the process of formulating the mapping from a given input to an output using Fuzzy logic. Fuzzy inference systems have been successfully applied in fields such as automatic control, data classification, decision analysis, expert systems, and computer vision. There are two types of Fuzzy inference systems that can be implemented.

- Mamdani-type and
- Sugeno-type.

These two types of inference systems vary somewhat in the way outputs are determined [10,11]. Mamdani-type inference requires finding the centroid of a two-dimensional shape by integrating across a continuously varying function.

Principal Elements to a Fuzzy logic controller are

- Fuzzification
- Rule base and Inference engine
- Defuzzification

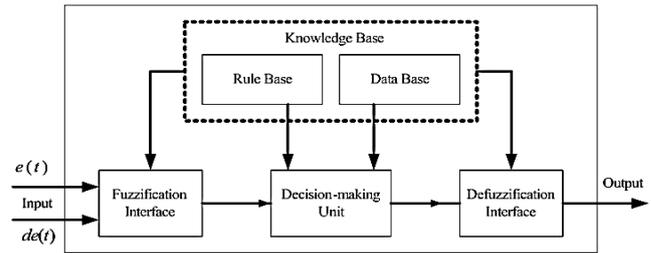


Fig. 6 Fuzzy Logic Controller block diagram

TABLE II FUZZY LOGIC CONTROLLER RULE TABLE

De/e	NVB	NB	NM	NS	Z	PS	PM	PB	PVB
NVB	PVB	PVB	PVB	PB	PM	PM	PS	Z	Z
NB	PVB	PVB	PB	PM	PS	PS	PS	Z	Z
NM	PVB	PB	PM	PS	PS	Z	Z	Z	NS
NS	PB	PM	PM	PS	PS	Z	Z	NS	NS
Z	PM	PM	PS	Z	Z	Z	NS	NS	NM
PS	PM	PS	PS	Z	NS	NS	NM	NM	NB
PM	PS	PS	Z	NS	NS	NM	NB	NB	NB
PB	PS	Z	Z	NS	NM	NM	NB	NVB	NVB
PVB	Z	Z	NS	NM	NM	NB	NB	NVB	NVB

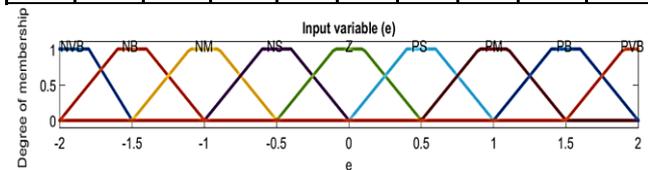


Fig. 7 Fuzzy logic first input variable, error

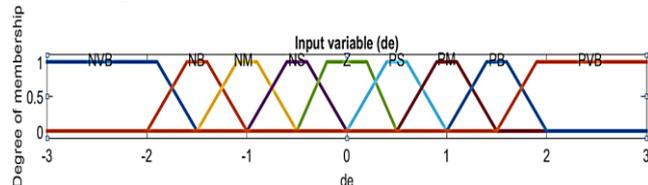


Fig. 8 Fuzzy logic second input variable, change of error

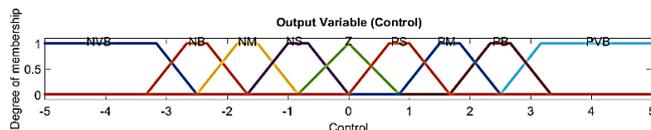


Fig. 9 Fuzzy logic output variable, control

A typical structure of a fuzzy logic controller is shown in Fig. 6. Using a pre-processor, the inputs that were in the form of crisp values generated from feedback error (e) and change of error (de) were conditioned in terms of multiplying by constant gains before entering into the main control block. The fuzzification block converts input data to degrees of membership functions and matches data with conditions of rules. From the rule based commands, the Mamdani type inference engine determined the capability of degree of employed rules and returned a Fuzzy set for defuzzification block where the Fuzzy output data were taken and crisp values were returned. The outputs of the Fuzzy sets were

converted to crisp values through centroid defuzzification method. The post processing block then converted these crisp values into standard control signals.

The rule table (TABLE II) is designed and used with a triangular membership function input-output in the fuzzy logic controller and was implemented in the simulation. These rules make control efforts based on several if-then statements about (e) and (de), i.e., if the error is equal Negative Big (NB) and change of error is equal to negative medium (NM), then the change in control (c) is positive big (PB). The numbers of these if-then statements were determined based on experiment and tuning of the system. Plots of fuzzy logic membership function for the two input variables (e) and (de) and the output (c) are shown in Fig. 7 to Fig. 9.

A. Advantages of Fuzzy Logic Controller

- Fuzzy Logic Controller (FLC) is an attractive choice when precise mathematical formulations are not possible.
- Allows imprecise or contradictory inputs. For example, it uses linguistic variables.
- Rule base or fuzzy sets can be easily modified.
- Relates input to output in linguistic terms, so easily understood.
- Cheaper because they are easier to design and increased robustness than other non-linear controller.
- Can achieve less overshoot and oscillation and doesn't require fast processors.
- It requires less data storage in the form of membership functions and rules than conventional look up table for non-linear controllers.

VI. SIMULATIONS AND RESULTS

The performances of the three designed controllers were simulated in Simulink with block diagram as shown in Fig. 10. A signal generator produces input references of step and sinusoidal function for each control blocks. The lead-lag and PID controller transfer function were implemented in the simulation followed by the DC motor dynamic model. The Fuzzy logic controller block process the inputs and output of Fuzzy inference engine and generate control signal.

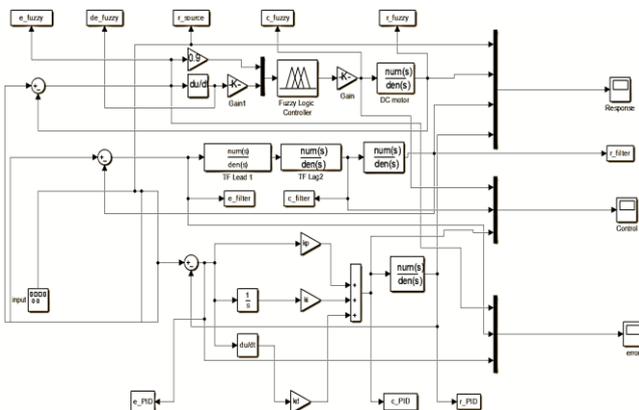


Fig. 10 Simulation diagram of PID, lead lag compensator and Fuzzy controllers for DC motor speed control

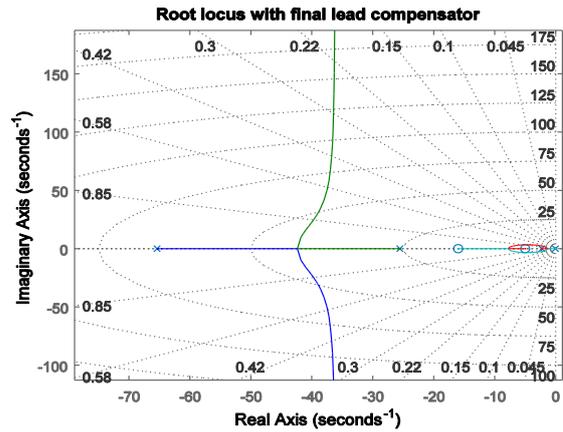


Fig. 11 Root locus of the DC motor system with lead compensator

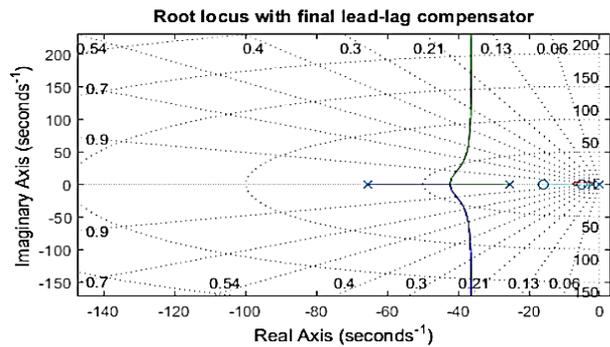


Fig. 12 Root locus of the DC motor system with final lead-lag compensator

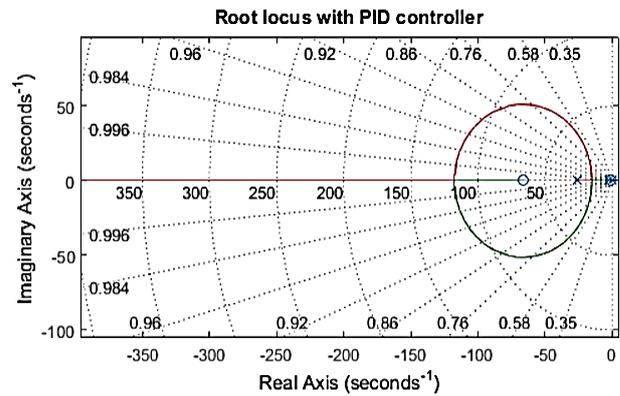


Fig. 13 Root locus of the DC motor system with PID controller

The root locus plot of the system with PID controller is also shown in Fig. 13 which proves that the design criteria with the desired poles locations have been satisfied.

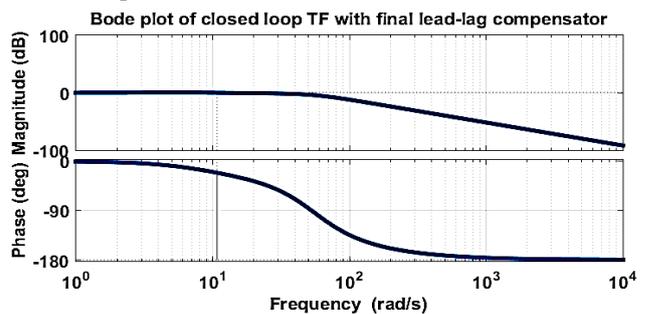


Fig. 14 Bode plot of closed loop TF with final lead-lag compensator, $G_m = \infty$ dB, $P_m = 158$ degree (at 10.8 rad/sec)

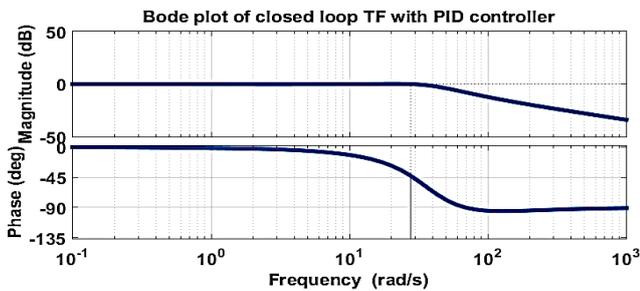


Fig. 15 Bode plot of closed loop TF with PID controller, $G_m = \infty$ dB, $P_m = 153$ degree (at 23.6 rad/sec)

According to the infinite gain and phase margin observed from the bode plots of the closed loop system in the presence of these controllers as shown in Fig. 14 and Fig. 15, the system will not become unstable with increasing gain.

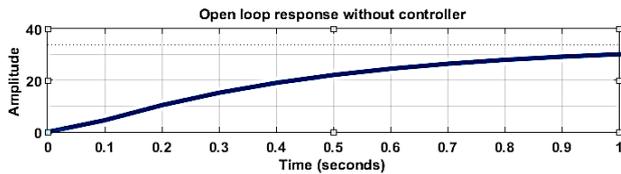


Fig. 16 Open loop step response without controller

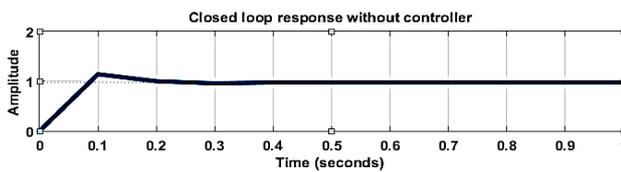


Fig. 17 Closed loop step response of DC motor without controller

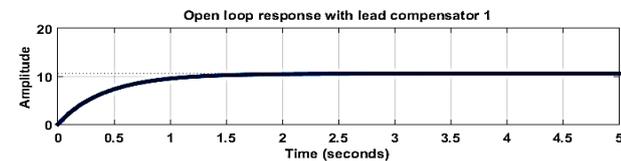


Fig. 18 Open loop step response of DC motor with first lead compensator

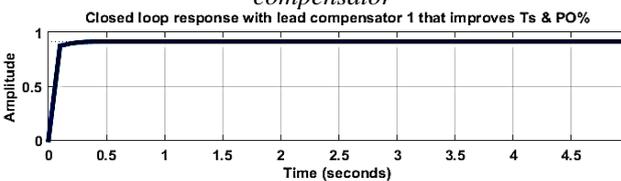


Fig. 19 Closed loop step response of DC motor with lead compensator

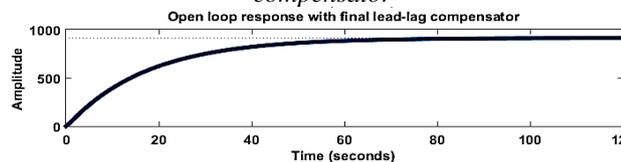


Fig. 20 Open loop step response of DC motor with final lead-lag compensator

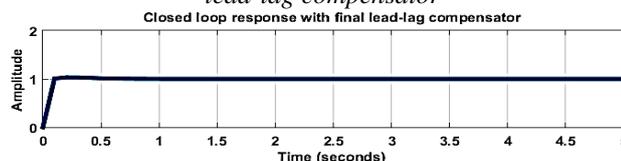


Fig. 21 Closed loop response of DC motor with final lead-lag compensator

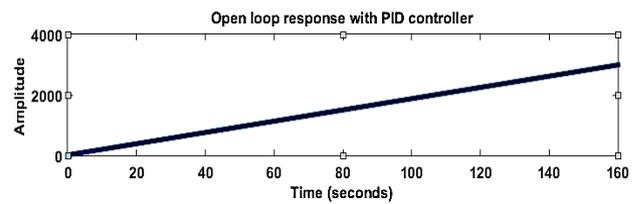


Fig. 22 Open loop step response of DC motor with PID controller

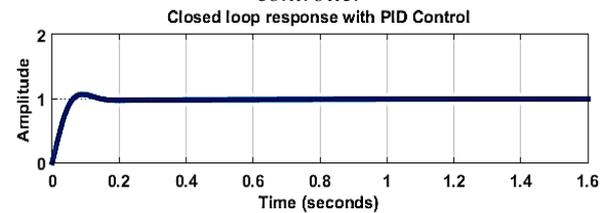


Fig. 23 Closed loop step response of DC motor with PID controller

The behavior of the open loop and closed loop response and the performance of the controllers were evaluated by input step functions and the plots are shown from Fig. 16 to Fig. 23.

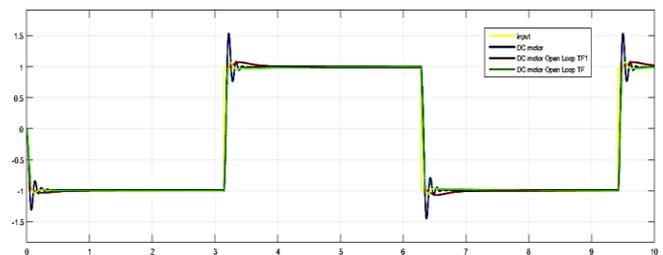


Fig. 24 For step response the performance comparison of the designed PID, lead-lag compensator and Fuzzy controllers

Plots of system responses and control signals are provided for the three controllers (lead lag compensator, PID and Fuzzy logic) design in Fig. 24.

Although the open loop system shows stability in nature, but the initial closed loop step response indicates a demand for a controller to improve rise time, settling time, overshoot and steady state error. All these performances were improved in the final closed loop response with lead-lag compensator, Fuzzy logic algorithm and PID controller with the results summarized in Table IV.

TABLE IV
 PERFORMANCE OF CONTROLLERS

Controller	Rise time(s)	Overshoot(%)	Settling time(s)
Lead Compensator	0.083	0	0.187
Final Lead-lag Compensator	0.0794	3.23	0.423
Conventional PID Controller	0.0456	6.46	0.422
Fuzzy Logic Controller	0.04	10.2	0.36

VII. CONCLUSION

In this paper, a PID controller, a lead-lag compensator filter, a lead compensator and a fuzzy logic controller for DC motor actuators have been designed. Simulation was performed to show the controllers' response for each proposed design. The research tool for this work was MATLAB and Simulink. The results showed that for step input, Fuzzy logic controller has better performance over conventional PID, lead compensator and lead-lag compensator design in terms of rise time, settling time and producing desired transient response.

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