

Edge-Coupled Stripline Bandpass Filter for 60 GHz Using Ansoft Designer

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Abstract— This paper covers trends and recent accomplishments in a wide range of circuits and systems topics that must be understood to design create for broadband wireless communication systems of the future. In this paper, we present some evolving applications of broadband wireless communications, and use tables and graphs to show research progress from the literature on various radio-frequencies (RF). We focus primarily on stripline based technologies, as these provide the best means of implementing very low-cost, highly integrated 60-GHz mm-wave edge-coupled stripline bandpass filter circuits. In addition, the paper illuminates characterization techniques that are required to competently design mm-wave devices in taclamplus substrate, and illustrates effects of the 60-GHz RF propagation channel for both in-building and outdoor use. For the proposed work we consider simulation using taclamplus substrate with dielectric constant of 2.1, Conductor Thickness 0.035 mm and Substrate Height 0.508 mm. The final conclusion which will describe the results to Ansoft Designer simulation results.

Index Terms— Stripline transmission line, Taclamplus dielectric substrates, Chebyshev band pass filter, V-band spectrum (60 GHz), Millimeter-wave wireless communication.

I. INTRODUCTION

In this paper design of an Edge-coupled bandpass filter realized in stripline technology is presented. The presented process includes the estimation of filter parameters using analytical formulas, the simulation of ideal and stripline transmission line models in a circuit simulator. These transmission lines are compact [1]. V-band uses millimeter-wave stepped-frequency radar operating from 60 GHz for sensing applications. The radar is implemented using coherent super-heterodyne scheme and completely realized using microwave and millimeter wave integrated circuits. The developed radar has been demonstrated for different sensing applications with high accuracy and resolution. In the United States, the band 38.6 - 40.0 GHz is used for licensed high-speed microwave data links, and the 60 GHz band can be used for unlicensed short range (1.7 km) data links with data throughputs up to 2.5 Gbit/s. It is used commonly in flat terrain. The 71-76, 81-86 and 92–95 GHz bands are also used for point-to-point high-bandwidth communication links. These frequencies, as opposed to the 60 GHz frequency, require a transmitting license in the US from the Federal Communications Commission (FCC), though they do not suffer from the effects of oxygen absorption as the 60 GHz does.

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The upcoming Wi-Fi standard IEEE 802.11ad will run on the 60 GHz (V-band) spectrum with data transfer rates of up to 7 Gb/s. Uses of the millimeter wave bands include point-to-point communications, intersatellite links, and point-to-multipoint communications. Because of shorter wavelengths, the band permits the use of smaller antennas than would be required for similar circumstances in the lower bands, to achieve the same high directivity and high gain. The immediate consequence of this high directivity, coupled with the high free space loss at these frequencies, is the possibility of a more efficient use of the spectrum for point-to-multipoint applications. Since a greater number of highly directive antennas can be placed in a given area than less directive antennas, the net result is higher reuse of the spectrum, and higher density of users, as compared to lower frequencies. It can be used for various sensing applications including Radio astronomy, high-frequency microwave radio relay, microwave remote, amateur radio, directed-energy weapon, and millimeter wave scanner [3].

In Europe, frequency is allocated for mobile in general in the 56–64 GHz band. No specific recommendation or decision has been issued yet in this mobile frequency band. However, the 56 – 64 GHz band is considered by CEPT as a main priority issue; in a recommendation document CEPT considers: “the high-frequency re-use achievable in the oxygen absorption band reduces the requirement for sophisticated frequency planning techniques and offers the possibility of a pan-European deregulated telecommunications environment for various low power, low cost, short-range applications” and “there is an urgent need to identify and harmonize civil requirements in the frequency range 56 – 64 GHz”. An important statement that has to be made here is that Europe should follow the US and Japan by opening a significant part of this band for unlicensed use, because license free is an important condition for promoting 60 GHz systems towards the market[3].

1.1 Stripline Model:

Stripline is a type of electrical transmission line which can be fabricated using printed circuit board technology, and is used to convey microwave-frequency signals. A stripline circuit uses a flat strip of metal which is sandwiched between two parallel ground planes. The insulating material of the substrate forms a dielectric. The width of the strip, the thickness of the substrate and the relative permittivity of the substrate determine the characteristic impedance of the strip which is a transmission line. As shown in the diagram Fig.1, the central conductor need not be equally spaced between the ground planes. In the general case, the dielectric material may be different above and below the central conductor. To prevent the propagation of unwanted modes, the two ground planes

must be shorted together. This is commonly achieved by a row of vias running parallel to the strip on each side. Like coaxial cable, stripline is non-dispersive, and has no cutoff frequency. Good isolation between adjacent traces can be achieved more easily than with microstrip. Stripline provides for enhanced noise immunity against the propagation of radiated RF emissions, at the expense of slower propagation speeds [1].

spacing will be forced to a minimum of this bit size. The taclamplus substrate sample available has a dielectric constant of 2.1 and a height of 0.508mm. A stripline chebyshev filter was generated with a center frequency of 60 GHz [6].

A bandpass filter is an important component must be found in the transmitter or receiver. Bandpass filter is a passive component which is able to select signals inside a specific bandwidth at a certain center frequency and reject signals in another frequency region, especially in frequency regions, which have the potential to interfere the information signals [4]. The development of the frequency bands in microwave filter, play an important role in many microwave applications. Through an investigation into and a subsequent implementation of filter theory, V-band (50-75 GHz) range filters design is developed in this report.

The spectrum is used for communications services, cellular radio services, and other commercial and private mobile radio operations services. There has been a particularly marked growth in the microwave communications industry in recent years. This has contributed to both very demanding performance specifications for filters and the commercial pressures for low cost, high volume and quick delivery [2].

In the process to fulfill these requirements there are several strategies taken in realization of the filters, for example, the choice of waveguide technology for the filter is preferred in respect to the minimal transmission loss (insertion loss).

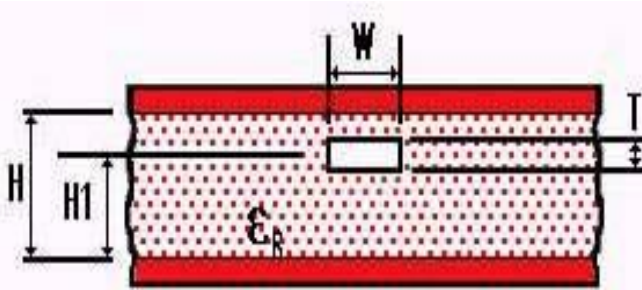


Fig. 1: Model used by Designer for Edge-Coupled Stripline Bandpass filter

After designing an acceptable model of the filter in the ideal case, the design must be realized in stripline technology to better represent how the filter will respond in a real world scenario. The substrate material taclamplus was chosen out of the available materials in the lab. The selection of taclamplus substrate dielectric material was based around the synthesis resulting in the highest separation of the first coupled section of all the available sample materials, as it was known that the rapid prototype machine has a minimum milling bit size and that trace

SPECIFICATIONS: TABLE 1.1

Specifications of Dielectric material Taclamplus substracts designed for microwave circuit applications requiring a high dielectric constant.		
1).	Input and Output Impedance:	Z = 50 Ohms
2).	Pass band ripple of	0.5 dB
3).	Filter Order:	n = 3
4).	Pass band Centre Frequency:	60 GHz
5).	Ripple Bandwidth:	8 GHz
Board and Substrate Properties:		
6).	Substrate:	Taclamplus
7).	Conductor Thickness:	0.035 mm
8).	Dielectric Constant:	2.1
9).	Loss Tangent:	0.0008
10).	Substrate Height:	0.508 mm

Table 1.1: Specifications of Edge-Coupled Stripline Bandpass Filter for 60 GHz [6]

1.2 Introducing Ansoft Designer:

Ansoft Designer is the first suite of design tools to fully integrate high-frequency, physics-based electromagnetic simulation, modeling, and automation into a seamless environment for circuit and system analysis. So whether your design challenge is a Bluetooth transceiver, a radar system, or an MMIC or RFIC, Ansoft Designer gives you complete

control over every design task from within one simple, unified environment. The key to this integration is Solver on Demand, a unique capability that orchestrates the use of multiple solvers while still giving you complete control. Ansoft Designer extends this automation and integration even further by enabling you to rapidly import work created in other types of design software as easily as if you created it within Ansoft Designer itself [13].

II. RESEARCH METHODOLOGY

In this paper Edge-coupled stripline bandpass filter (BPF) development with the assistance of the Richards-Kuroda Transformation method, on the basis of the known Chebyshev-Lowpass Filter, is presented. This suggested filter consist of four Edge-coupled striplines. The use of the 56–64 GHz frequency band is a promising solution for Gigabit short range wireless communication systems. Up to 8 GHz unlicensed bandwidth was allocated around the world for various communication applications and the standardization is developing under the IEEE standard 802.15.3c, 802.15.11ad, and the European Computer Manufacturers Association (ECMA) standard 387. Another advantage beside the high unlicensed bandwidth is the fact to have low interference with other electrical systems in the vicinity. This is due to the high amount of energy absorption by oxygen molecules around 60 GHz [6, 9].

The bandpass filter could either be realized using lumped component or distributed component. Lumped components consists of discrete elements like inductors, capacitors etc. Distributed elements consist of transmission line section which simulates various inductors and capacitors values. At very high frequency the practical inductors and capacitors losses their intrinsic characteristics. So it is hard to realized filters with lumped elements. Transmission lines are easy to implement and compact at this frequency. Transmission lines are needed for connecting various circuit elements and systems. Therefore for microwave frequency (>3GHz) passive filter is usually realized using distributed circuit element such as transmission line. Open wire and Coaxial lines are commonly used for circuits operating at low frequencies. On the other hand Stripline, Microstrip line and Waveguides are operating at radio and microwave frequencies. In the design, three kinds of transmission lines were normally used: Waveguide Striplines, and Microstrip lines. Waveguides systems are bulky and expensive. Low-power and cheaper alternatives are Stripline and Microstrip. These transmission lines are compact. Edge-coupled stripline is used instead of microstrip line as stripline does not suffer from dispersion and its propagation mode is pure TEM mode. Hence it is the preferred structured for Edge-coupled Stripline [4, 5, 7-15].

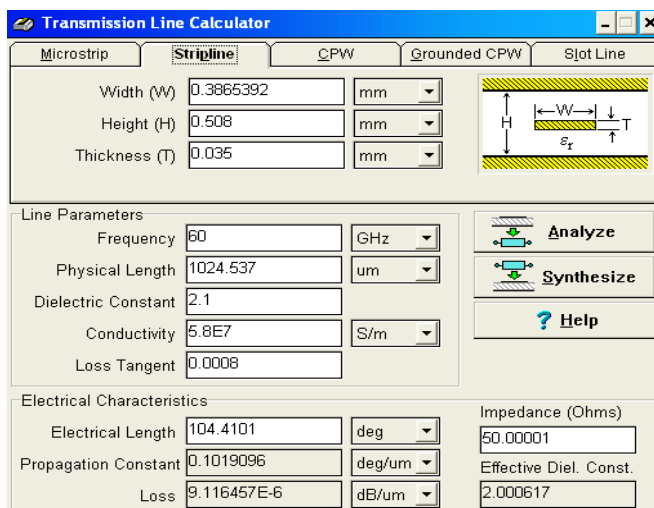


Fig. 2: Transmission Line Calculator Result Response Of 3rd Order Edge-Coupled Stripline Bandpass Filter

In analysis mode, the physical width w , and length L , of the transmission line are entered and the program calculates the resulting effective dielectric constant ϵ_{re} the characteristic impedance Z_0 , the electrical length, and the loss of the line. In synthesis mode, the desired characteristic impedance and electrical length are entered and the program calculates the required width and length for the transmission line. The substrate characteristics and operating frequency must be specified for both analysis and synthesis.

The proposed filter is designed by following steps.

First step: Determining the order (n) to be used.

Second step: Finding the corresponding low-pass prototype structure and convert into bandpass filter.

Third step: Find out the distributed realization using J inverter and Y_0 is the characteristic admittance of the connecting transmission line.

Fourth step: Calculate the characteristic impedances of (Z_{oe}) even-mode and (Z_{oo}) odd-mode of the parallel-coupled stripline transmission line based on the mathematical formulation and compare with simulated value.

Fifth step: Determine the Effective dielectric constant ϵ_{re} and length L measurement based on the mathematical formulation.

Six step: Determine the w , s , and L using simulated layout.

Seven step: Analysis & Design are completed by using simulation software.

2.1 Design of Chebyshev Band Pass Filter:

The BPF circuit is simulated with Ansoft Designer software in order to predict the performance of the filter. Few parameters in the circuit are analyzed and have a good relationship to microwave theory. An optimization process has been introduced along the simulation procedure focusing on the filter dimension in order to improve the response of the filter. Refer to the filter tables given in D.M Pozar and G. L. Mather [2] to find the following coefficients for a third order chebyshev filter. Normalized element values for 0.5 dB ripple low-pass chebyshev filter given in was $g_0 = 1$, $g_1 = 1.5963$, $g_2 = 10967$, $g_3 = 1.5963$, $g_4 = 1.000$ for simulated third order filter [14,15].

2.2 Determining the Number of Sections (n):

The bandpass filter is designed to have a 0.5dB equal-ripple response, with an attenuation of 50 dB at 60GHz. From the amplitude versus normalized frequency graph in [1-2], the number of stages required, N is found to be 3. The bandpass filter is realized as a cascade of $n+1$ coupled line sections as shown in Fig. 3. The sections are numbered from left to right. The source is connected at the left and the load is connected to the right. The filter could be reversed without affecting the response [15].

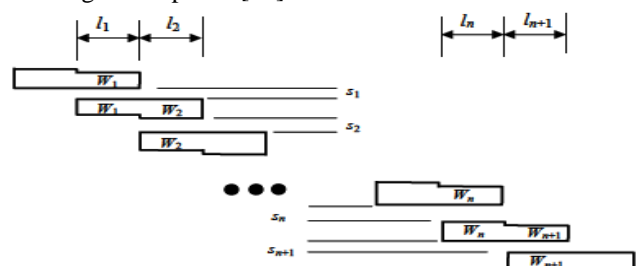


Fig. 3: Bandpass filter is realized as a cascade of $n+1$ coupled line sections

J	$J_{j,j+1}/Y_0$	$(Z_{oe})_{j,j+1}(\Omega)$ (Derived results)	$(Z_{oo})_{j,j+1}(\Omega)$ (Derived results)	$(Z_{oe})_{j,j+1}(\Omega)$ (Simulated results)	$(Z_{oo})_{j,j+1}(\Omega)$ (Simulated results)
0	.3622	74.6711	38.4492	75.21	38.37
1	.1583	59.1674	43.3382	59.53	43.15
2	.1583	59.1674	43.3382	59.53	43.15
3	.3622	74.6711	38.4492	75.21	38.37

This filter type is known as parallel-coupled filter. The strips are arranged parallel close to each other, so that they are coupled with certain coupling factors.

2.3 Even and Odd Modes in a Coupled Transmission Line:

Calculation of Odd and Even Resistances to design the strip line filter, an approximate calculation is made based on the design equations. The no of stages (n) = 3. The characteristic impedance Z0 is typically 50 Ohms. The unitary bandwidth BW is given by

where $BW = \frac{(\omega_2 - \omega_1)}{\omega_0}$ is the fractional

(1) III. $FBW = \frac{(64 \times 10^9 - 56 \times 10^9)}{60 \times 10^9} \approx .1333$ (1)

(2) $\frac{J_{01}}{Y_0} = \sqrt{\frac{\pi FBW}{2 g_0 g_1}}$ (2)

(3) $\frac{J_{j,j+1}}{Y_0} = \frac{\pi FBW}{2} \frac{1}{\sqrt{g_j g_{j+1}}}$ for j=1 to n-1

(3) $\frac{J_{n,n+1}}{Y_0} = \sqrt{\frac{\pi FBW}{2 g_n g_{n+1}}}$

(5) Where g_0, g_1, \dots, g_n are the element of a ladder-type low-pass prototype with a Normalized cutoff $\Omega_c = 1$, and FBW is the fractional bandwidth of band-pass filter. $J_{j,j+1}$ are the characteristic admittances of J-inverters and Y_0 is the characteristic admittance of the terminating lines. The equation above will be use in end-coupled line filter because the both types of filter can have the same low-pass network representation. However, the implementation will be different [1, 4-15].

To realize the J-inverters obtained above, the even- and odd-mode characteristic impedances of the coupled strip line band pass filter are determined by

$(Z_{oe})_{j,j+1} = \frac{1}{Y_0} [1 + \frac{J_{j,j+1}}{Y_0} + (\frac{J_{j,j+1}}{Y_0})^2]$ for j=0 to n (6)

$(Z_{oo})_{j,j+1} = \frac{1}{Y_0} [1 - \frac{J_{j,j+1}}{Y_0} + (\frac{J_{j,j+1}}{Y_0})^2]$ for j=0 to n (7)

(1) Table 1.2: Circuit Design Parameters of the 3rd Order, Parallel-Coupled Stripline Bandpass Filter

2.4 Effective Dielectric Constant And Length Measurement : For W=0.3865 mm (Standard value):

$\epsilon_{re} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \frac{1}{\sqrt{1 + \frac{12h}{W}}}$ (8)

$\epsilon_{re} = \frac{2.1+1}{2} + \frac{2.1-1}{2} \frac{1}{\sqrt{1 + \frac{12 \times .508}{0.3865}}} = 1.8598 mm$ (9)

Thus the required length, $\ell = \frac{\lambda_g}{4} = \frac{c}{4f\sqrt{\epsilon_{re}}} = \frac{3 \times 10^8}{4 \times 60 \times 10^9 \times \sqrt{1.8598}} = 0.9166 mm$ (10)

The length of the resonator requires for third order coupled line filter will have four, quarter wave-length segments. So final filter length is $L = (n+1) \times \ell = (3+1) \times 0.9166 = 3.664 mm$ (11)

IV. SIMULATED RESULT & DISCUSSION

We discuss the results obtained from Ansoft software. The frequency sweep for the linear simulation of the advanced numerical models was performed from 33 to 50 GHz in 0.1 GHz steps.

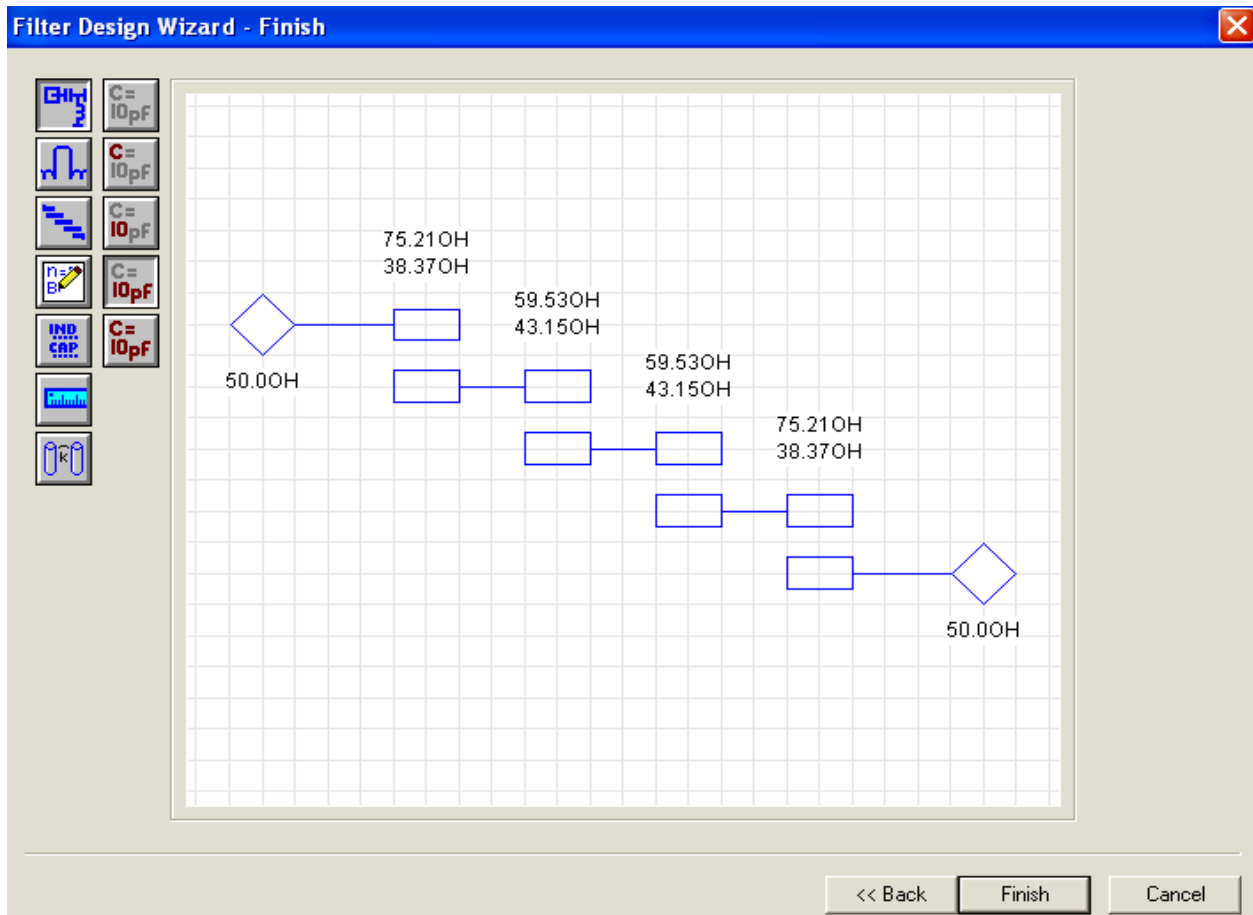


Fig.4. Software result of odd and even impedances response of 3rd order edge-coupled stripline bandpass filter

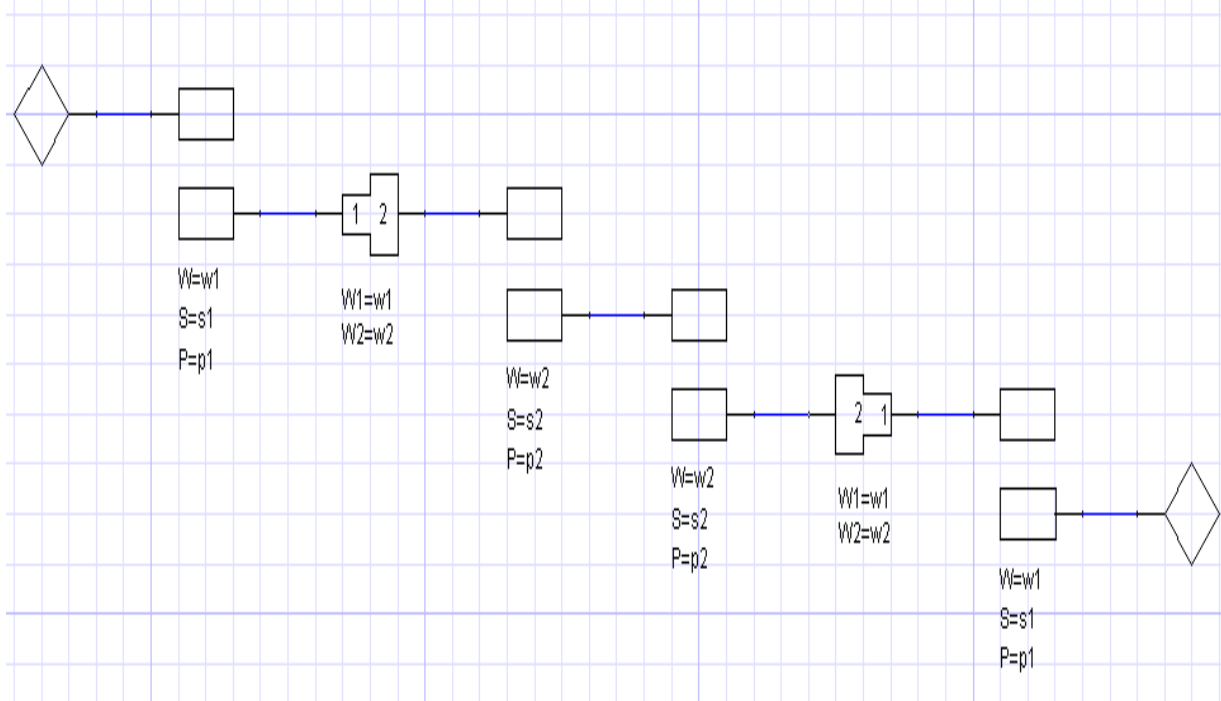


Fig. 5: Tuned Chebyshev Band Pass Filter Made From Physical Model Configuration of 3rd Order Edge-Coupled Stripline Bandpass Filter

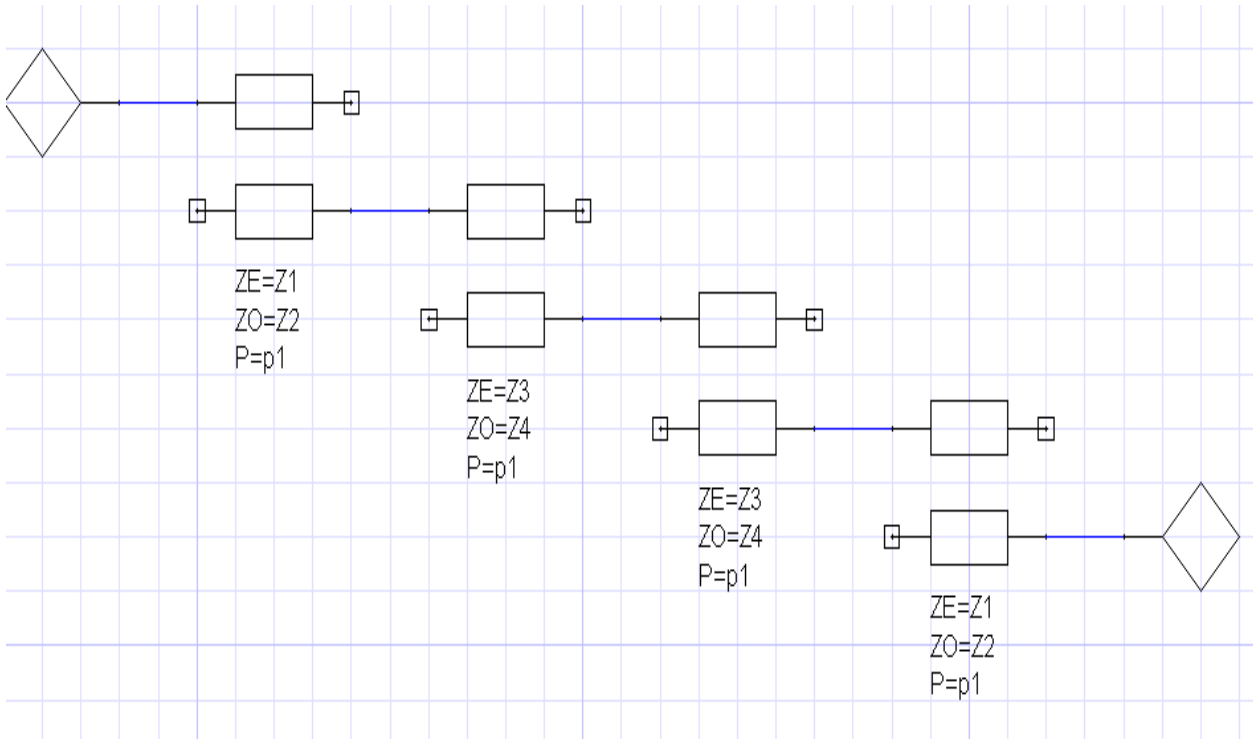


Fig. 6: Electrical Model Configuration of 3rd Order Edge-Coupled Stripline Bandpass Filter

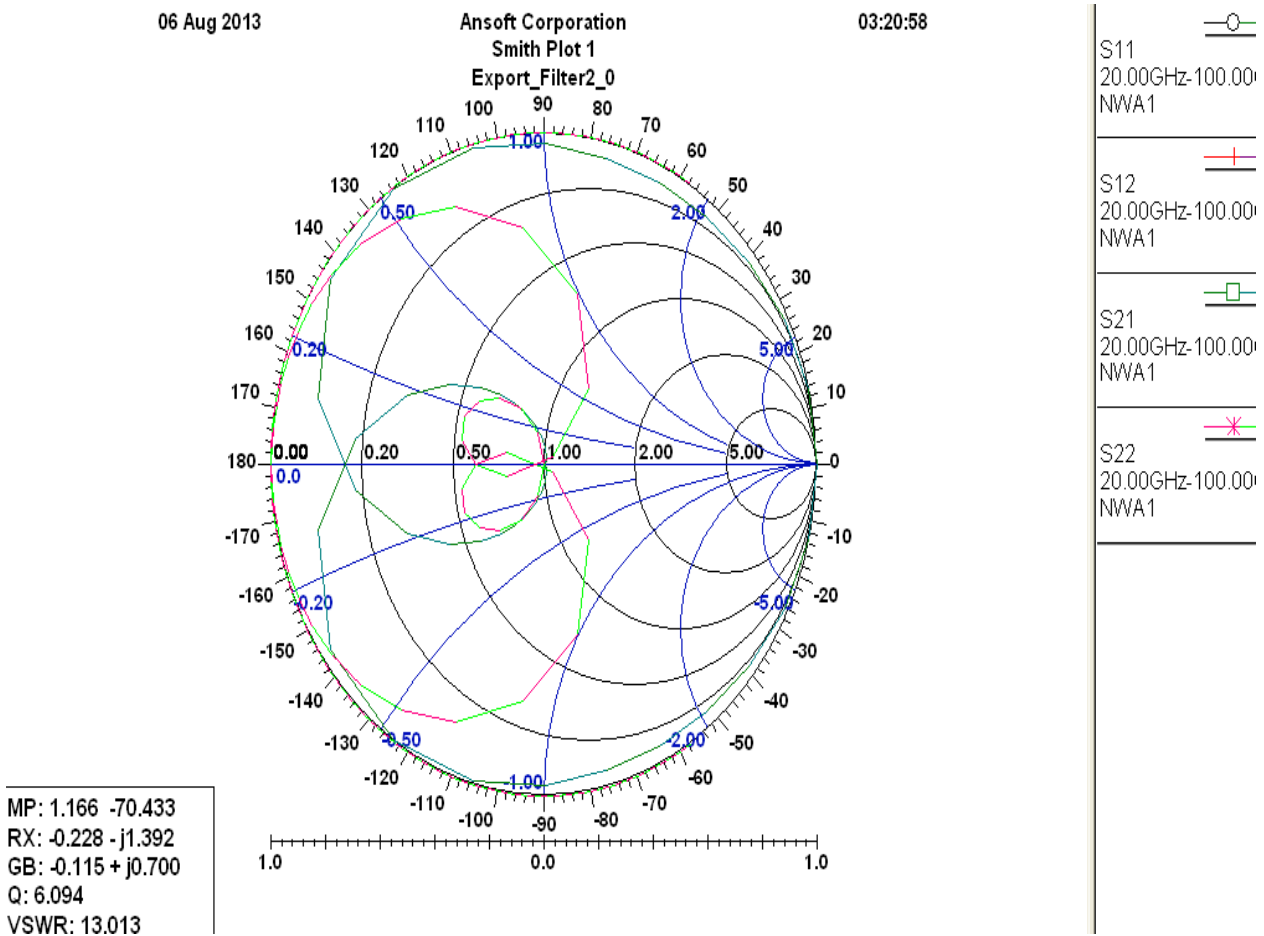


Fig. 7: Simulated Smith Chart Result of 3rd Order Edge-Coupled Stripline Bandpass Filter

Smith chart to be used for problems involving any characteristic or system impedance which is represented by

the center point of the chart. The most commonly used normalization impedance is 50 ohms. Once an answer is

obtained through the graphical constructions described in Fig. 7, it is straightforward to convert between normalised impedance (or normalised admittance) and the corresponding unnormalized value by multiplying by the characteristic impedance (admittance).

Reflection coefficients can be read directly from the chart as they are unitless parameters. Any actual reflection coefficient must have a magnitude of less than or equal to unity so, at the test frequency, this may be expressed by a point inside a circle of unity radius. The Smith chart is actually constructed on such a polar diagram.

The Smith chart scaling is designed in such a way that reflection coefficient can be converted to normalised impedance or vice versa. Using the Smith chart, the

normalised impedance may be obtained with appreciable accuracy by plotting the point representing the reflection coefficient treating the Smith chart as a polar diagram and then reading its value directly using the characteristic Smith chart scaling. This technique is a graphical alternative to substituting the values in the equations [8].

Smith chart is a set of constant resistance and constant reactance circle draw on complex gamma plane. One especially point and that is center of smith chart at that is intersection of $r=1$ and $x=0$ on the line. This mark a point on smith chart represents match condition so the impedance lines on the center which cross ponds to the magnitude of reflection coefficient zero.

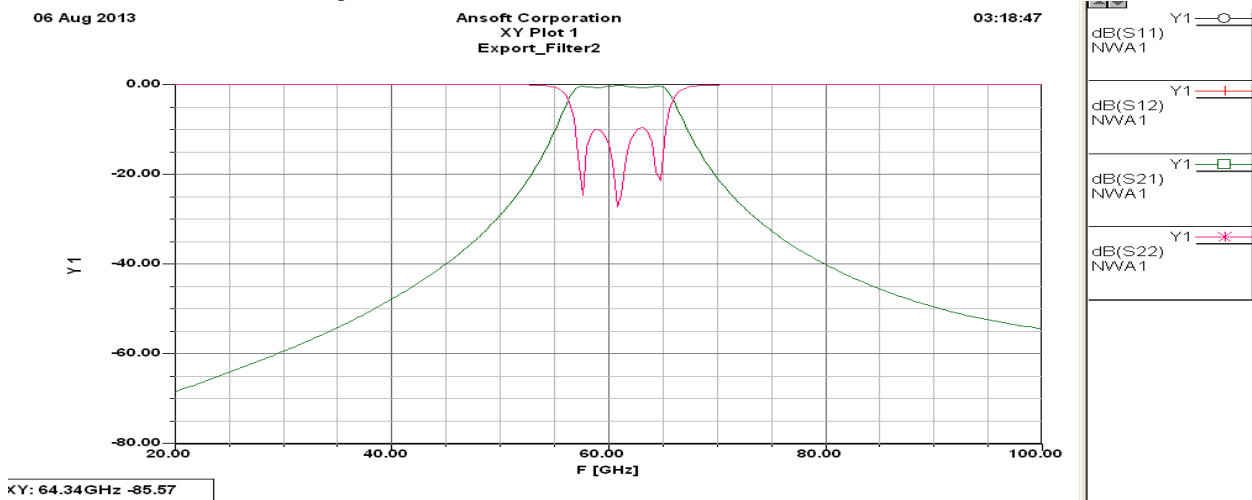


Fig. 8: Simulated result for Physical model insertion loss and return loss response of 3rd order edge-coupled stripline bandpass filter

Return loss is the loss of signal power resulting from the reflection caused at a discontinuity in a transmission line. Return loss is related to both standing wave ratio (SWR) and reflection coefficient (Γ). Increasing return loss corresponds to lower SWR. Return loss is a measure of how well devices or lines are matched. A match is good if the return loss is high. A high return loss is desirable and results in

a lower insertion loss. Return loss is used in modern practice in preference to SWR because it has better resolution for small values of reflected wave. Insertion loss is a figure of merit for an electronic filter and this data is generally specified with a filter. Insertion loss is defined as a ratio of the signal level in a test configuration without the filter installed ($|V_1|$) to the signal level with the filter installed ($|V_2|$).

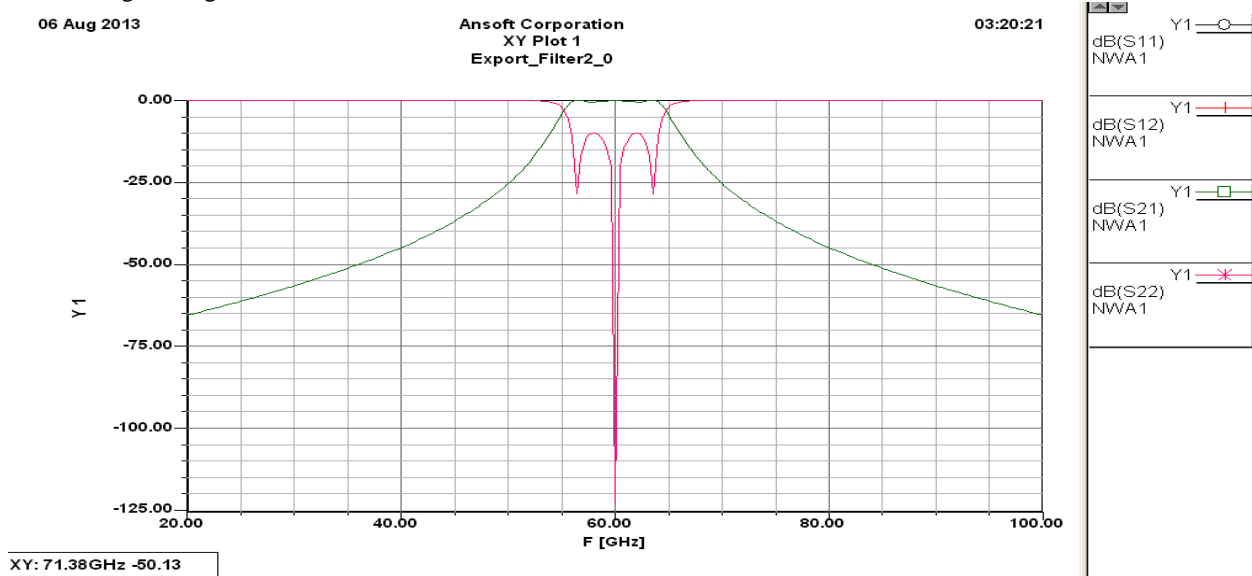


Fig. 9: Simulated result for Electrical model insertion loss and return loss response of 3rd order edge-coupled stripline bandpass filter

The two parameters insertion loss and return loss are to analyze to obtain a good performance of filter. A good filter will be high return loss and small insertion loss ripple in pass band. The simulated insertion loss is less than 0.1 dB. The return loss is greater than 50 dB at center frequency. Reflection regarding in accuracies present in simulators result and simulation result show that the filter operation is optimum over the frequency range 56 GHz to 64 GHz which is best in this range. The simulated insertion loss is less than 0.1 dB in pass band. Also the response is flat and uniform over the entire pass-band. In addition, reflection coefficient is 0.00001 which is nearly equal to 0 and a perfect match exists. The filter is almost matched to the characteristic impedance (Z_0), 50 Ohms. Also it is observed that the phase varies linearly with frequency.

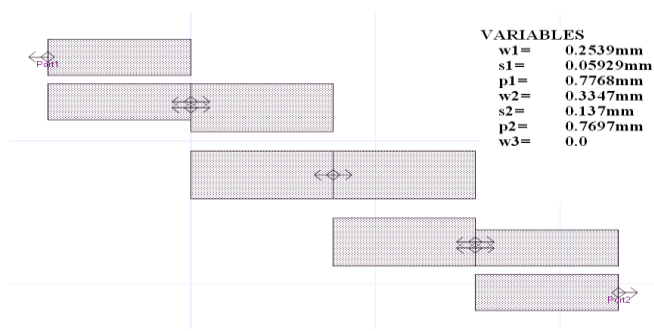


Fig.10: Detail dimensions of the simulated layout model result of 3rd order stripline edge-coupled bandpass filter

The Layout of the filter is generated from the schematic design Fig. 10. A pair of parallel-coupled striplines with certain width and separation distance will deliver a pair of characteristic impedances, the even mode and the odd mode ones. We can determine the width of parallel-coupled strip line band pass filter w and the distance between them s . The process is visualized in layout Fig.10. According to layout we get $w_1=0.2539$ mm and $s_1=0.0592$ mm. The same data will be also used for the fourth resonator.

V. CONCLUSION:

The overall performance of edge-coupled stripline bandpass filter can often judged by its simulated insertion loss and return loss result response. Design an edge-coupled stripline band-pass filter centered at 60 GHz with 8 GHz bandwidth based on chebyshev approximation. The two parameters insertion loss and return loss are to analyze to obtain a good performance of filter. A good filter will be high return loss and small insertion loss ripple in pass band. The filter is simulated with Ansoft Designer 2.2 software to simulated insertion loss is less than 0.1 dB in the desired pass band and the simulated return loss is greater than 30 dB at center frequency. Reflection coefficient is nearly equal to 0, perfect match. The tool developed here is compared to two industry standard software packages, Ansoft Designer. Ansoft Designer v2.2 simulation software was used to accurately arrive at the final design. Filters are an essential part of communication and radar systems and are key items in the performance and cost of such systems, especially in the increasingly congested spectrum. Experimental implementation of this work involves the taclamplus substrate

with dielectric constant of 2.1 dielectric characterizations at microwave frequencies. Third-order edge-coupled stripline band pass filter is used in order to realize these objectives. If more-accurate frequency response is required, more stages should be used. A coupled line bandpass filter was successfully designed by direct calculation and by using a CAD design tool.

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